Entropy stable schemes based on high order modal discontinuous Galerkin formulations

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- Instability: quadrature error + loss of the discrete chain rule in space.



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Entropy stability for nonlinear problems uses the chain rule

 Generalizes energy stability to nonlinear systems of conservation laws (Burgers', shallow water, compressible Euler, MHD).

$$\frac{\partial \boldsymbol{u}}{\partial t} + \frac{\partial \boldsymbol{f}(\boldsymbol{u})}{\partial x} = 0 \qquad x \in [-1,1].$$

• Continuous entropy inequality: given a scalar convex entropy function S(u) and "entropy potential" $\psi(u)$,

$$\int_{-1}^{1} \mathbf{v}^{T} \left(\frac{\partial \mathbf{u}}{\partial t} + \frac{\partial \mathbf{f}(\mathbf{u})}{\partial x} \right) = 0, \qquad \left| \mathbf{v} = \frac{\partial S}{\partial \mathbf{u}} \right|$$
$$\implies \frac{\partial}{\partial t} \int_{-1}^{1} S(\mathbf{u}) + \left(\mathbf{v}^{T} \mathbf{f}(\mathbf{u}) - \psi(\mathbf{u}) \right) \Big|_{-1}^{1} \leq 0.$$

Proof of entropy inequality relies on chain rule, integration by parts.

Continuous entropy stability: Hughes et al. 1986, Zakerzadeh/May, Fernandez/Nguyen/Peraire, Williams, ...

Talk outline

- 1 Entropy stable nodal DG and summation-by-parts
- 2 Entropy stable modal DG formulations
- 3 Numerical experiments
 - Triangular and tetrahedral meshes
 - Quadrilateral and hexahedral meshes
 - Hybrid and non-conforming meshes

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Nodal DG, summation-by-parts (SBP), flux differencing



Gauss-Lobatto nodes mimic integration by parts algebraically

$$\boldsymbol{Q} = \boldsymbol{B} - \boldsymbol{Q}^{T}, \qquad \boldsymbol{Q} = \boldsymbol{M} \boldsymbol{D}, \qquad \boldsymbol{M}$$
 diagonal mass matrix.

■ Nodal "collocation" over a single element:

$$\boldsymbol{M} \frac{\mathrm{d}\boldsymbol{u}}{\mathrm{dt}} + \boldsymbol{Q}\boldsymbol{f}(\boldsymbol{u}) = 0 \implies \boldsymbol{M}_{ii} \frac{\mathrm{d}\boldsymbol{u}_i}{\mathrm{dt}} + \sum_j \boldsymbol{Q}_{ij}\boldsymbol{f}(\boldsymbol{u}_j) = 0.$$

• Let $\boldsymbol{f}_{S}(\boldsymbol{u}_{i},\boldsymbol{u}_{j}) = \frac{1}{2} (\boldsymbol{f}(\boldsymbol{u}_{i}) + \boldsymbol{f}(\boldsymbol{u}_{j})) = (\boldsymbol{F}_{S})_{ij}$. Collocation equiv. to

$$\boldsymbol{M}_{ii}\frac{\mathrm{d}\boldsymbol{u}_{i}}{\mathrm{dt}}+\sum_{i}\boldsymbol{Q}_{ij}2\boldsymbol{f}_{S}\left(\boldsymbol{u}_{i},\boldsymbol{u}_{j}\right)=0\quad=$$

$$\boldsymbol{M}\frac{\mathrm{d}\boldsymbol{u}}{\mathrm{d}\mathrm{t}}+2\left(\boldsymbol{Q}\circ\boldsymbol{F}_{\boldsymbol{S}}\right)\boldsymbol{1}=\boldsymbol{0}.$$

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J. Chan (Rice CAAM)

4/3/19 4/21

DG: derive local formulation (one element) with interface flux f^*

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Trick: use Tadmor's entropy conservative numerical flux for f_S, f^*

$$f_{S}(\boldsymbol{u}, \boldsymbol{u}) = f(\boldsymbol{u}), \quad (\text{consistency})$$
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Benefits of entropy stability (conservation)



(b) Entropy conservative flux, T = .7

Figure: Compressible Euler shock vortex interaction: 200×100 degree N = 4elements, 4th order explicit RK time-stepping, no limiters or artificial viscosity.

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(a) Local Lax-Friedrichs flux, T = .3 (b) Local Lax-Friedrichs flux, T = .7

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Entropy stable modal DG formulations

Modal formulations: general bases and quadrature



Assume degree 2N volume + surface quadratures $(\mathbf{x}_i^q, \mathbf{w}_i^q)$, $(\mathbf{x}_i^f, \mathbf{w}_i^f)$, and basis functions $\phi_i(\mathbf{x})$. Define interpolation and weight matrices

$$(\boldsymbol{V}_q)_{ij} = \phi_j(\boldsymbol{x}_i^q), \qquad (\boldsymbol{V}_f)_{ij} = \phi_j(\boldsymbol{x}_i^f),$$
$$\boldsymbol{W} = \operatorname{diag}(\boldsymbol{w}^q), \qquad \boldsymbol{W}_f = \operatorname{diag}(\boldsymbol{w}^f).$$

• Discretize $P_N : L^2 \rightarrow P^N$, yields a quadrature-based projection matrix

$$(P_N u, v) = (u, v) \quad \forall v \in P^N \implies P_q = M^{-1} V_q^T W.$$

Entropy stable modal DG formulations

Quadrature-based "finite difference" matrices



Matrix D_q^i : evaluates *i*th derivative of L^2 projection P_N at x^q . $D_q^i = V_q D^i P_q, \qquad D^i \quad \text{exactly differentiates polynomials.}$

• Generalized summation-by-parts: let $\boldsymbol{Q}_i = \boldsymbol{W} \boldsymbol{D}_q^i$ and $\boldsymbol{E} = \boldsymbol{V}_f \boldsymbol{P}_q$

$$\boldsymbol{Q}_i + \boldsymbol{Q}_i^T = \boldsymbol{E}^T \boldsymbol{B}_i \boldsymbol{E}, \qquad \boldsymbol{B}_i = \boldsymbol{W}_f \operatorname{diag}(\boldsymbol{n}_i)$$

$$\Longrightarrow \int_{\widehat{D}} \frac{\partial P_N u}{\partial x_i} v + \int_{\widehat{D}} u \frac{\partial P_N v}{\partial x_i} = \int_{\partial \widehat{D}} (P_N u) (P_N v) \widehat{n}_i.$$

Problems with generalized SBP on multiple elements



Coupling between quadrature nodes on neighboring elements.

Re-deriving the local DG formulation with GSBP operators:

$$\boldsymbol{M} rac{\mathrm{d}\boldsymbol{u}}{\mathrm{dt}} + 2\left(\boldsymbol{Q}\circ\boldsymbol{F}_{\mathcal{S}}\right)\mathbf{1} = 0.$$

The presence of the interpolation matrix *E* increases inter-element coupling, complicates imposition of BCs.

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Entropy stable modal DG formulations

A "decoupled" SBP operator

■ Goal: SBP property without *E* in the boundary terms

$$\boldsymbol{Q}_{N}=\left[egin{array}{ccc} \boldsymbol{Q}-rac{1}{2}\boldsymbol{E}^{T}\boldsymbol{B}\boldsymbol{E} & rac{1}{2}\boldsymbol{E}^{T}\boldsymbol{B}\ -rac{1}{2}\boldsymbol{B}\boldsymbol{E} & rac{1}{2}\boldsymbol{B}\end{array}
ight],$$

• If $\boldsymbol{Q} + \boldsymbol{Q}^T = \boldsymbol{E}^T \boldsymbol{B} \boldsymbol{E}$, then the block matrix \boldsymbol{Q}_N satisfies

$$\boldsymbol{Q}_N + \boldsymbol{Q}_N^T = \begin{bmatrix} \boldsymbol{0} & \\ & \boldsymbol{B} \end{bmatrix} \sim \int_{-1}^1 \frac{\partial P_N u}{\partial x} v + u \frac{\partial P_N v}{\partial x} = u v |_{-1}^1.$$

• \boldsymbol{Q}_N approximates $f \frac{\partial g}{\partial x}$ by \boldsymbol{u} using data at $\boldsymbol{x} = [\boldsymbol{x}_{\mathrm{vol}}, \boldsymbol{x}_{\mathrm{face}}]$

$$\boldsymbol{M} \boldsymbol{u} = \begin{bmatrix} \boldsymbol{V}_q \\ \boldsymbol{V}_f \end{bmatrix}^T \operatorname{diag}(\boldsymbol{f}) \boldsymbol{Q}_N \boldsymbol{g}, \qquad \boldsymbol{f}_i, \boldsymbol{g}_i = f(\boldsymbol{x}_i), g(\boldsymbol{x}_i).$$

Reduces to traditional SBP operator under appropriate quadrature.

Entropy stable schemes using decoupled SBP operators

Replace SBP operator with decoupled SBP operator

$$\boldsymbol{M}\frac{\mathrm{d}\boldsymbol{u}}{\mathrm{dt}} + \left(\left(\boldsymbol{Q} - \boldsymbol{Q}^{T}\right) \circ \boldsymbol{F}_{S}\right)\boldsymbol{1} + \boldsymbol{B}\boldsymbol{f}^{*} = \boldsymbol{0}.$$

■ **F**_S is the matrix of flux evaluations between solution values at *both* volume and face nodes using entropy projection:

$$(\boldsymbol{F}_{S})_{ij} = \boldsymbol{f}_{S}(\widetilde{\boldsymbol{u}}_{i},\widetilde{\boldsymbol{u}}_{j}), \qquad \widetilde{\boldsymbol{u}} = \text{ evaluate } \boldsymbol{u}(P_{N}\boldsymbol{v}(\boldsymbol{u})).$$

 Semi-discrete scheme is verifiably entropy conservative for inexact quadrature! Add appropriate interface dissipation (e.g. Lax-Friedrichs, HLLC) for entropy stability.

Chan (2018). On discretely entropy conservative and entropy stable discontinuous Galerkin methods. Parsani et al. (2016), Entropy Stable Staggered Grid Discontinuous Spectral Collocation Methods

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Talk outline

1 Entropy stable nodal DG and summation-by-parts

2 Entropy stable modal DG formulations

3 Numerical experiments

- Triangular and tetrahedral meshes
- Quadrilateral and hexahedral meshes
- Hybrid and non-conforming meshes

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Numerical experiments Triangu

Triangular and tetrahedral meshes

Smooth isentropic vortex and curved meshes in 2D/3D



• "Split" form of derivatives on curved elements for entropy stability.

$$J\frac{\partial u}{\partial x_i} = \sum_{j=1}^d J\frac{\partial \widehat{x}_j}{\partial x_i}\frac{\partial u}{\partial \widehat{x}_j} = \frac{1}{2}\sum_{j=1}^d \left(J\frac{\partial \widehat{x}_j}{\partial x_i}\frac{\partial u}{\partial \widehat{x}_j} + \frac{\partial}{\partial \widehat{x}_j}\left(J\frac{\partial \widehat{x}_j}{\partial x_i}u\right)\right).$$

■ Discrete geometric conservation law (GCL) now a necessary condition.

Visbal and Gaitonde (2002). On the Use of Higher-Order Finite-Difference Schemes on Curvilinear and Deforming Meshes. Chan, Hewett, and Warburton (2016). Weight-adjusted discontinuous Galerkin methods: curvilinear meshes.

Smooth isentropic vortex and curved meshes in 2D/3D



 L^2 errors for 2D/3D isentropic vortex at T = 5 on affine, curved meshes.

Visbal and Gaitonde (2002). On the Use of Higher-Order Finite-Difference Schemes on Curvilinear and Deforming Meshes. Chan, Hewett, and Warburton (2016). Weight-adjusted discontinuous Galerkin methods: curvilinear meshes.

Inviscid Taylor-Green vortex



Figure: Isocontours of z-vorticity for Taylor-Green at t = 0, 10 seconds.

- Simple turbulence-like behavior (generation of small scales).
- Inviscid Taylor-Green: tests robustness w.r.t. under-resolved solutions.

https://how4.cenaero.be/content/bs1-dns-taylor-green-vortex-re1600.

Inviscid Taylor-Green vortex: robust w.r.t. under-resolution



Kinetic energy dissipation rate $-\frac{\partial \kappa}{\partial t}$ for $N = 3, h = \pi/8, CFL = .25$ (tet meshes).

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- Advantage of hexahedra vs. tetrahedra: tensor product structure.
- (N + 1)-point Gauss quadrature reduces to a collocation scheme.
- Reduces computational costs from $O(N^6)$ to $O(N^4)$ in 3D.



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Mixed quadrilateral-triangle meshes



- GSBP property lost if surface quadrature insufficiently accurate.
- Skew-symmetric formulation remains entropy stable under "weak" GSBP property, relaxed requirements on quadrature accuracy.

Chan (2019). Skew-symmetric entropy stable modal discontinuous Galerkin formulations.

Numerical results: mixed triangle-quadrilateral meshes



The skew-symmetric formulation guarantees entropy stability for all combinations of Lobatto and Gauss volume and surface quadratures.

Non-conforming interfaces



(a) Conforming surface quadrature nodes



(b) Non-conforming surface nodes

- Volume/surface nodes interact through $f_S(u_i, u_j)$ and interpolation.
- Fix: weakly couple conforming+non-conforming faces using a mortar.

Numerical results: non-conforming meshes



(a) Coarse non-conforming mesh

(b) Sub-optimal rates if under-integrated

The skew-symmetric formulation guarantees entropy stability for both Lobatto and Gauss quadratures, but Gauss is more accurate.

Summary and future work

- Entropy stable high order "modal" DG: flexibility in choosing basis and quadrature, improved accuracy on curved meshes.
- Current work: ROMs, strong shocks, positivity preservation.
- This work is supported by DMS-1719818 and DMS-1712639.

Thank you! Questions?



Chan (2019). Skew-symmetric entropy stable modal discontinuous Galerkin formulations.
 Chan, Del Rey Fernandez, Carpenter (2018). Efficient entropy stable Gauss collocation methods.
 Chan, Wilcox (2018). On discretely entropy stable weight-adjusted DG methods: curvilinear meshes.
 Chan (2018). On discretely entropy conservative and entropy stable discontinuous Galerkin methods.

J. Chan (Rice CAAM)

Entropy stable DG

Additional slides

Decoupled SBP operators add boundary corrections



• Equivalent to a variational problem for a polynomial $u(\mathbf{x}) \approx f \frac{\partial g}{\partial x}$.

$$\int_{-1}^{1} u(\mathbf{x})v(\mathbf{x}) = \int_{-1}^{1} f \frac{\partial P_N g}{\partial x}v + (g - P_N g) \frac{(fv + P_N(fv))}{2} \Big|_{-1}^{1}$$

Flux differencing: recovering split formulations

Entropy conservative flux for Burgers' equation

$$f_{S}(u_{L}, u_{R}) = \frac{1}{6} \left(u_{L}^{2} + u_{L}u_{R} + u_{R}^{2} \right).$$

• Flux differencing: let $u_L = u(x), u_R = u(y)$

$$\frac{\partial f(u)}{\partial x} \Longrightarrow 2 \frac{\partial f_{\mathcal{S}}(u(x), u(y))}{\partial x} \bigg|_{y=x}$$

Recovering the Burgers' split formulation

$$f_{\mathcal{S}}(u(x), u(y)) = \frac{1}{6} \left(u(x)^2 + u(x)u(y) + u(y)^2 \right)$$
$$2\frac{\partial f_{\mathcal{S}}(u(x), u(y))}{\partial x} \Big|_{y=x} = \frac{1}{3}\frac{\partial u^2}{\partial x} + \frac{1}{3}u\frac{\partial u}{\partial x} + \frac{1}{3}u^2\frac{\partial 1}{\partial x}.$$

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1D compressible Euler equations

- Inexact Gauss-Legendre-Lobatto (GLL) vs Gauss (GQ) quadratures.
- Entropy conservative (EC) and dissipative Lax-Friedrichs (LF) fluxes.
- No additional stabilization, filtering, or limiting.



Conservation of entropy: semi-discrete vs. fully discrete

$$\Delta S(oldsymbol{u}) = |S(oldsymbol{u}(x,t)) - S(oldsymbol{u}(x,0))| o 0$$
 as as $\Delta t o 0$.



Solution and change in entropy $\Delta S(\boldsymbol{u})$ for entropy conservative (EC) and Lax-Friedrichs (LF) fluxes (using GQ-(N + 2) quadrature).

1D sine-shock interaction

• (N+2)-point Gauss needs a smaller CFL (.05 vs .125) for stability.



1D sine-shock interaction

• (N+2)-point Gauss needs a smaller CFL (.05 vs .125) for stability.



Loss of control with the entropy projection

- For (N + 1)-Lobatto quadrature, $\widetilde{\boldsymbol{u}} = \boldsymbol{u} (P_N \boldsymbol{v}) = \boldsymbol{u}$ at nodal points.
- For (N + 2)-Gauss, discrepancy between v(u) and L^2 projection.
- Still need positivity of thermodynamic quantities for stability!



Over-integration is ineffective without L^2 projection



Figure: Numerical results for the Sod shock tube for N = 4 and K = 32 elements. Over-integrating by increasing the number of quadrature points does not improve solution quality.

2D Riemann problem

- Uniform 64 \times 64 mesh: N = 3, CFL .125, Lax-Friedrichs stabilization.
- No limiting or artificial viscosity required to maintain stability!
- Periodic on larger domain ("natural" boundary conditions unstable).



Non-conforming interfaces and SBP mortars



- Define appropriate interpolation operators $\boldsymbol{E}_m, \widetilde{\boldsymbol{E}}_m$ between conforming and non-conforming (mortar) nodes.
- Modify the skew-symmetric formulation as follows:

$$\boldsymbol{M}\frac{\mathrm{d}\boldsymbol{u}}{\mathrm{dt}} + \sum_{i=1}^{d} \begin{bmatrix} \boldsymbol{V}_{q} \\ \boldsymbol{V}_{f} \end{bmatrix}^{T} \begin{bmatrix} \boldsymbol{Q}_{i} - \boldsymbol{Q}_{i}^{T} & \boldsymbol{E}^{T}\boldsymbol{B}_{i} \\ -\boldsymbol{B}_{i}\boldsymbol{E} \end{bmatrix} + \boldsymbol{E}^{T}\boldsymbol{B}_{i}\boldsymbol{f}_{i}^{*} = 0.$$

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Non-conforming interfaces and SBP mortars



- Define appropriate interpolation operators $\boldsymbol{E}_m, \widetilde{\boldsymbol{E}}_m$ between conforming and non-conforming (mortar) nodes.
- Rewrite as modification of numerical flux.

$$\widetilde{\boldsymbol{f}}_{i}^{*} = \widetilde{\boldsymbol{E}}_{m} \boldsymbol{f}_{i}^{*} + \left(\widetilde{\boldsymbol{E}}_{m} \circ \boldsymbol{F}_{S}^{sm}\right) \boldsymbol{1} - \widetilde{\boldsymbol{E}}_{m} \left(\boldsymbol{E}_{m} \circ \boldsymbol{F}_{S}^{ms}\right) \boldsymbol{1}$$